REPORT ON

SOIL INVESTIGATION FOR C/ GIRL,BOY HOSTEL EDUCATIONAL BHAWAN, PRINCIPAL-CUM-STAFF QUARTER BUILDING(G+4) AT PTEC MOKAMA,PATNA,BIHAR.

Submitted to
CHIEF ENGINEER
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PREFACE

The present report on sub-soil investigation was carried out as per Chief Engineer, BSEIDC, Patna letter no BSEIDC/TECH/1960/2018-7139 dated 02.09.2023.

The entire investigation process was broadly divided into two category –one field work and second was laboratory work.

Field work includes conducting SPT ,Dynamic cone test, collection of disturbed as well as undisturbed soil samples from different location and different depth of sub-soil strata.

It was tried to get information from local people to get an idea about variation of water table during different season of year and also to get first hand information about type of foundation usually provided in the locality.

We thanks Prof. M.P.Jakhanwal (Retired) ,M.Tech ,Ph.D. ,Muzaffarpur Institute of Technology, Muzaffarpur for his valuable advice during laboratory test and during preparation of report.

Client's help is gratefully acknowledged in providing Bore hole locations, cooperation and guidance during finalization of report.

We belief that the present report will serve the purpose, for which sub-soil investigation has been carried out.

Subodh kumar Sinha

SUBODH KUMAR SINHA
Partner, Shamvwi Consultant

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REPORT ON SUB-SOIL INVESTIGATION FOR THE C/O OF GIRL,BOY HOSTEL EDUCATIONAL BHAWAN, PRINCIPAL-CUM-STAFF QUARTER BUILDING(G+4) AT PTEC MOKAMA,PATNA,BIHAR

1. INTRODUCTION

The objective of subsoil investigation reported here in, were taken up, to find out the nature of subsoil at the site of the proposed construction and to recommend the type or types of foundation suitable for it and the corresponding allowable bearing capacity.

The necessary field tests were carried out at the site. Soil samples from various depths in the different bore holes were collected, transported, carefully to the laboratory and tested to determine the engineering properties of the soil.

Based on the test results, certain recommendation were made and given in this report, regarding the type of foundation suitable for the proposed project and the allowable bearing capacity for certain sizes thereof.

2. TOPOGRAPHY

The land in question was even.

3. FIELD WORK

The field work consists of boring, soil sampling and conduct of Standard penetration tests and Dynamic cone penetration tests.

3.1 BORING

An appropriate number of boreholes of adequate depth were sunk at suitable spots as per direction of Engineer-in-charge. The details of the boreholes are given in table-1.

Table 1: Details of bore holes

DIAMETER OF BORE MM	DEPTH M	BORE HOLE
150	10.5	3 Bore Holes (BH-1 to BH-3)

The borings were kept dry while advancing through partially saturated soil. The position of water table in a borehole was recorded at least 48 hours after the stopping of the boring operation.

For boring below ground water level, the borehole was kept filled with water upto that level during boring.

3.2 SAMPLING

Undisturbed & disturbed samples were collected at different depth/where change of strata occurred. Identification slips were provided both inside and outside the tube.
On arrival in laboratory, the identification slips were checked against the boring and sampling records.
Samples were extracted from the tubes just before testing.

3.3 STANDARD PENETRATION TEST

This test was performed in the boreholes at interval of depth of 1.5m, or at the change of starta/ as per IS: 2131 of 1963.

3.4 DYNAMIC CONE PENETRATION TEST

This test was performed when a bore hole could not be advanced to desired depth due to caving- in of the soil, or when it was felt necessary to supplement the information gained from SPT. This test was performed, as per

relevant IS code till high value of penetration resistance was encountered or till desired depth of investigation was reached, at which stage the test was stopped.

4. LABORATORY TEST

Lab. Test was performed to determine the following properties of soil samples as per relevant I.S. code.
(a) Natural moisture content.
(b)Bulk density.
(c) Atterberg' s limits (on fine grained soil only)
(d) Grain size analysis.
(e) Specific gravity.
(f) Shear test.
(i) Unconfined/triaxial compression tests for fine-grained soils.
(ii) Direct shear test for coarse-grained soils.
(g)Consolidation tests for fine grained soils.
(h) Organic content, chemical test etc.
(i) pH of soil and water.
(j) Free swell Index
(k)Crushing strength test (uniaxial)

4.1 SAMPLE EXTRACTION & PREPARATION OF TEST SPECIMENS

Samples for different tests were prepared as per method described in relevant IS code/as per method described in standard book.

4.2 ROUTINE CLASSIFICATION TESTS.

Tests for the determination of natural moisture content, bulk density, Atterberg's limit, grain size distribution and specific gravity were performed as per IS code on representative disturbed soil samples, wherever felt necessary. The results were used in classifying the soils of different strata as per IS code 1498-1970.

5.0 PRESENTATION OF TEST RESULT

Results were presented in table form on the following pages.

6.0 METHOD FOR CALCLATION OF ALLOWABLE BEARING CAPACITY

6.1 COHESIVE SOIL

Net ultimate bearing capacity was calculated as per IS-6403-1981.
$qd = cNcScDcIc$

qd = net ultimate bearing capacity

Nc=5.14

Sc=1 for strip footing

Dc=1+0.2*D/B

Ic=1 for vertical loading

c= cohesion obtained through unconfined compression test for depth of 2B/3 below the foundation.

Settlement criteria

$S=H/(1+eo)*Cc*\log((po+p1)/po)$

S= settlement

H=thickness of compressible layer

eo=initial void ratio

po=initial effective pressure

p1=pressure increment

Cc=compression index

6.2 Soil with the value of c &θ

Net ultimate bearing capacity was calculated as per IS 6403-1981

$Qd=cNcScDcIc+q(Nq-1)SqDqIq+0.5R*BNr*Sr*Dr*Ir*w'$

For local shear failure

$\text{Tan } \underline{\theta}'=0.67*\text{Tan}\underline{\theta}$

$C'=2*c/3$

Sc=Sq=Sr=1 for strip footing

$Dc=1+0.2*(D/B)*\text{Tan}(45+\underline{\theta}/2)$

Ic=Iq=Ir=1 for vertical loading

$Dq=Dr=1+0.1*(D/B)\text{Tan}(45+\underline{\theta}/2)$

q=(R-Rw)*D

M= moisture content

R= bulk density of soil

Rw=unit weight of water

L.L.= liquid limit

P.L.=plastic limit

S.L.= shrinkage limit

D=depth below ground level

Settlement criteria

The net allowable bearing capacity for a permissible settlement of 25mm, was obtained by

teng's formula

Qna=3.5*(N-3)*{(B+0.3)/2*B}*{(B+0.3)/2*B}*w'*Fd

N= corrected N

Fd=1+D/B less than or equal to 2

7.0 METHOD FOR CALCLATION OF CAPACITY OF CAST-IN-SITU PLANE PILE AS PER BIS 2911 Part I/Sec 2-1979

7.1 COHESIVE SOIL

Net ultimate bearing capacity of pile is given by :

Q=Ap*Nc*Cp +a * C* As

Ap=cross sectional area of pile toe in cm2

Nc=Bearing capacity factor usually taken as 9

Cp=average cohesion at pile tip in Kg/cm

.

a=reduction factor

C= average cohesion throughout the length of pile in kg/cm2

As= surface area of pile shaft in cm2

8.0 METHOD FOR CALCLATION OF CAPACITY OF CAST-IN-SITU PLANE PILE AS PER BIS 2911 Part III-1980

8.1 COHESIVE SOIL

Net ultimate bearing capacity of pile is given by :

Q=Ap*Nc*Cp +Aa **Nc*** C'a + C'a*As'+α*Ca*As

Ap=cross sectional area of pile toe in cm2

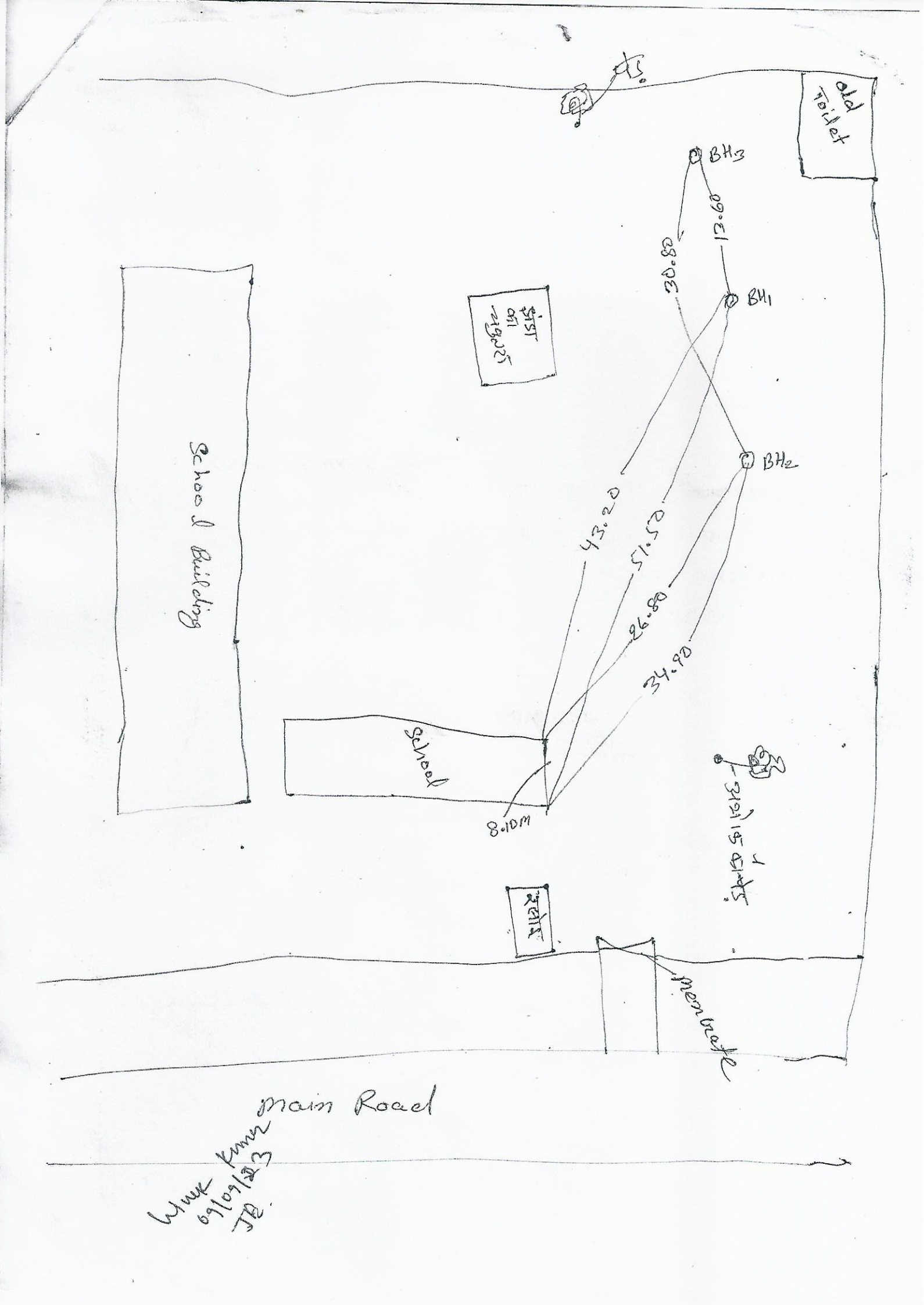
Nc=Bearing capacity factor usually taken as 9

Cp= cohesion of soil around toe.

α=reduction factor

$Aa=\pi*(Du^2 - D^2)/4$

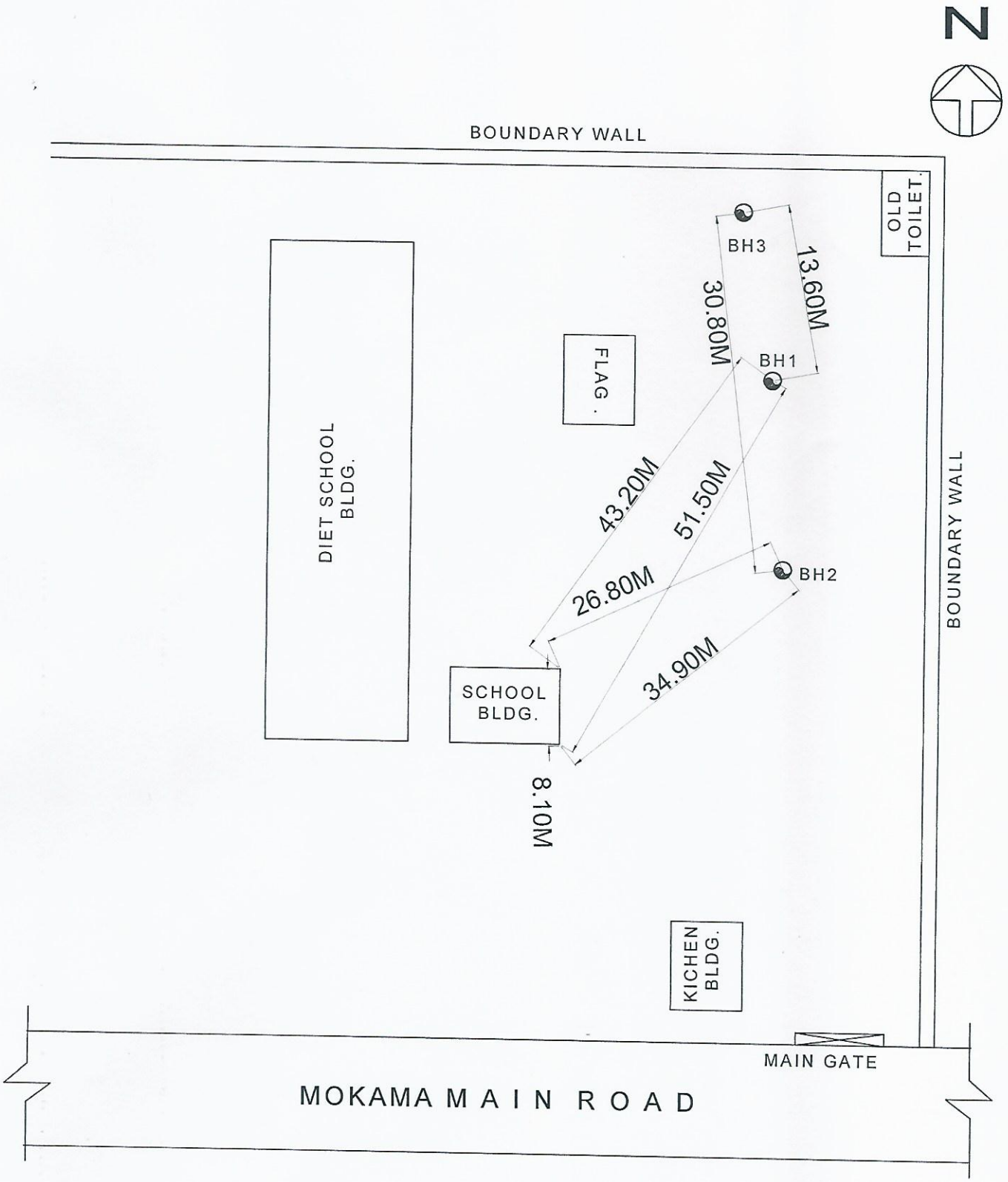
C'a= average cohesion around under ream
Du=dia of under-ream,D=dia of pile
As= surface area of pile shaft in cm2
As=surface area of stem
A's=surface area of the cylinder circumscribing the under ream.


Old Toilet
BH3
BH1
BH2
30.80
13.60
43.20
51.50
26.80
34.90
8.10m
School Building
School
Main Road
Menhole

LEAD CHART OF DISTANCE COVEREDED

SL-NO	NAME OF SCHOOL	DISTANCE COVEREDED	LEAD CHART
(1)	Diet Building Arato Diet Building mokama	160 KM	
(2)	Diet Building mokama to Patna Lab	100 KM	

MOKAMA


N
BOUNDARY WALL
OLD TOILET.
BH3
13.60M
30.80M
BH1
FLAG .
DIET SCHOOL BLDG.
43.20M
51.50M
BH2
26.80M
34.90M
SCHOOL BLDG.
8.10M
BOUNDARY WALL
KICHEN BLDG.
MAIN GATE
MOKAMA MAIN ROAD

SHAMVWI CONSULTANT ,414,J.T.C.,FRASER ROAD, PATNA	NAME OF PROJECT : SOIL INVESTIGATION FOR CONSTRUCTION OF GIRL,BOY HOSTEL EDUCATIONAL BHAWAN, PRINCIPAL-CUM-STAFF QUARTER BUILDING(G+4) AT PTEC MOKAMA,PATNA,BIHAR	BORING DATES	TERMINATION DEPTH :10.5M	TABLE NO :2
		START :09.09.2023	WATER TABLE DEPTH : 3.2m	BORE HOLE NO :BH1
		FINISH :09.09.2023		

SAMPLE NO	DEPTH OF SAMPLE	STANDARD PENETRATION RESISTANCE CURVE (5 10 20) OBSERVED VALUE	CORRECTED VALUE	VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	ATTERBERG'S LIMITS LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	DENSITY BULK DENSITY (gm/cm3)	DRY DENSITY(gm/cm3)	NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST TYPE OF TEST	COHESION c (kg/cm2)	ANGLE OF FRICTION IN DEGREE	CONSISTENCY LIMITS VOID RATIO eo	COMPRESSION INDEX Cc	UNCONFINED COMPRESSION TEST ,q kg/cm2	COEFFICIENT OF VOLUME COMPRESSIBILITY Mv cm2/kg
DS	G.L.																					
UDS 1				Blackish clay CL																		
SPT1	1.5	14			0.1	13.50	86.4		35	16	19	1.98	1.67	18.8	2.65	UUT	0.3	20.0				
UDS 2				Blackish clay CL																		
SPT2	3	6			0.10	17.30	82.6		35	16	19	1.98	1.67	18.8	2.65	UUT	0.30	20.00				
UDS 3				Blackish clay CL																		
SPT3	4.5	10			0.30	16.80	82.9		35	17	18	1.98	1.63	21.5	2.65	UUT	0.40	20.00				
UDS 4				Blackish clay CL																		
SPT4	6	21			0.10	17.40	82.5		35	16	19	1.98	1.64	20.8	2.65	UUT	0.60	18.00				

UUT : UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST

UCT : UNCONFINED COMPRESSION SHEAR TEST

DST : DIRECT SHEAR TEST

! SAMPLE SLIPED

~ TEST ON REMOULDED SAMPLE

UDS : UNDISTURBED SAMPLE

SPT : STANDARD PENETRATION TEST VALUE

NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m2

SHAMVWI CONSULTANT ,414,J.T.C.,FRASER ROAD, PATNA	NAME OF PROJECT : SOIL INVESTIGATION FOR CONSTRUCTION OF GIRL,BOY HOSTEL EDUCATIONAL BHAWAN, PRINCIPAL-CUM-STAFF QUARTER BUILDING(G+4) AT PTEC MOKAMA,PATNA,BIHAR	BORING DATES START :09.09.2023 FINISH :09.09.2023	TERMINATION DEPTH :10.5M WATER TABLE DEPTH : 3.2m	TABLE NO :3 BORE HOLE NO :BH1

SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE	VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST			CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST ,q kg/cm2	COEFFICIENT OF VOLUME COMPRESSIBILITY Mv cm3/kg
		OBSERVED VALUE	CORRECTED VALUE	5 10 20		GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm3)	DRY DENSITY(gm/cm3)			TYPE OF TEST	COHESION c (kg/cm2)	ANGLE OF FRICTION IN DEGREE	VOID RATIO eo	COMPRESSION INDEX Cc		
UDS 5					Yellowish Reddish Silty clay CL																		
SPT5	7.5	22				0.3	3.7	96.0		35	19	16	1.99	1.65	20.3	2.65	UUT	0.8	13.0				
UDS 6					Yellowish Reddish Silty clay CL																		
SPT6	9.0	23				0.20	3.80	96.0		35	19	16	1.99	1.62	22.80	2.65	UUT	0.90	13.00				
UDS 7					Yellowish Reddish Silty clay CL																		
SPT7	10.5	26				0.10	3.70	96.2		35	19	16	1.99	1.61	23.60	2.65	UUT	0.90	13.00				

UUT : UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST

UCT : UNCONFINED COMPRESSION SHEAR TEST

DST : DIRECT SHEAR TEST

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~ TEST ON REMOULDED SAMPLE

UDS : UNDISTURBED SAMPLE

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NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m2

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		START :09.09.2023	WATER TABLE DEPTH : 3.2m	BORE HOLE NO :BH2
		FINISH :09.09.2023		

SAMPLE NO	DEPTH OF SAMPLE	OBSERVED VALUE	CORRECTED VALUE	STANDARD PENETRATION RESISTANCE CURVE 5 10 20	VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST			CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST ,q kg/cm2	COEFFICIENT OF VOLUME COMPRESSIBILITY Mv cm3/kg
						GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm3)	DRY DENSITY(gm/cm3)			TYPE OF TEST	COHESION c (kg/cm2)	ANGLE OF FRICTION IN DEGREE	VOID RATIO eo	COMPRESSION INDEX Cc		
DS	G.L.																						
UDS 1					Blackish clay CL																		
SPT1	1.5	14				0.0	13.20	86.8		35	16	19	1.98	1.66	19.5	2.65	UUT	0.3	20.0	0.83	0.11		
UDS 2					Blackish clay CL																		
SPT2	3	6				0.00	17.60	82.4		35	16	19	1.98	1.67	18.6	2.65	UUT	0.30	20.00				
UDS 3					Blackish clay CL																		
SPT3	4.5	10				0.30	16.80	82.9		35	17	18	1.98	1.62	22.3	2.65	UUT	0.40	20.00				
UDS 4					Blackish clay CL																		
SPT4	6	21				0.10	17.40	82.5		35	16	19	1.98	1.62	22.5	2.65	UUT	0.60	18.00				

UUT : UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST

UCT : UNCONFINED COMPRESSION SHEAR TEST

DST : DIRECT SHEAR TEST

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		START :09.09.2023	WATER TABLE DEPTH : 3.2m	BORE HOLE NO :BH2
		FINISH :09.09.2023		

SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE	VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST			CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST ,q kg/cm2	COEFFICIENT OF VOLUME COMPRESSIBILITY Mv cm3/kg
		OBSERVED VALUE	CORRECTED VALUE	5 10 20		GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm3)	DRY DENSITY(gm/cm3)			TYPE OF TEST	COHESION c (kg/cm2)	ANGLE OF FRICTION IN DEGREE	VOID RATIO eo	COMPRESSION INDEX Cc		
UDS 5					Yellowish Reddish Silty clay CL																		
SPT5	7.5	22				0.5	3.6	95.9		35	19	16	1.99	1.62	22.8	2.65	UUT	0.8	13.0				
UDS 6					Yellowish Reddish Silty clay CL																		
SPT6	9.0	23				0.50	3.70	95.8		35	19	16	1.99	1.62	22.50	2.65	UUT	0.90	13.00				
UDS 7					Yellowish Reddish Silty clay CL																		
SPT7	10.5	26				0.40	3.80	95.8		35	19	16	1.99	1.62	22.80	2.65	UUT	0.90	13.00				

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UCT : UNCONFINED COMPRESSION SHEAR TEST

DST : DIRECT SHEAR TEST

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UDS : UNDISTURBED SAMPLE

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		START :10.09.2023	WATER TABLE DEPTH : 3.2m	BORE HOLE NO :BH3
		FINISH :10.09.2023		

SAMPLE NO	DEPTH OF SAMPLE	OBSERVED VALUE	CORRECTED VALUE	STANDARD PENETRATION RESISTANCE CURVE (5 — 10 — 20)	VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST			CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST ,q kg/cm2	COEFFICIENT OF VOLUME COMPRESSIBILITY Mv cm3/kg
						GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm3)	DRY DENSITY(gm/cm3)			TYPE OF TEST	COHESION c (kg/cm2)	ANGLE OF FRICTION IN DEGREE	VOID RATIO eo	COMPRESSION INDEX Cc		
DS	G.L.																						
UDS 1					Blackish clay CL																		
SPT1	1.5	13				0.5	13.60	85.9		35	16	19	1.98	1.67	18.6	2.65	UUT	0.3	20.0				
UDS 2					Blackish clay CL																		
SPT2	3	7				0.10	17.30	82.6		35	16	19	1.98	1.65	19.8	2.65	UUT	0.30	20.00				
UDS 3					Blackish clay CL																		
SPT3	4.5	9				0.60	17.20	82.2		35	17	18	1.98	1.61	22.8	2.65	UUT	0.40	20.00				
UDS 4					Blackish clay CL																		
SPT4	6	20				0.40	17.60	82.0		35	16	19	1.98	1.61	23.2	2.65	UUT	0.60	18.00				

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UCT : UNCONFINED COMPRESSION SHEAR TEST

DST : DIRECT SHEAR TEST

! SAMPLE SLIPED

~ TEST ON REMOULDED SAMPLE

UDS : UNDISTURBED SAMPLE

SPT : STANDARD PENETRATION TEST VALUE

NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m2

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		START :10.09.2023	WATER TABLE DEPTH : 3.2m	BORE HOLE NO :BH3
		FINISH :10.09.2023		

SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE	VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST			CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST ,q kg/cm2	COEFFICIENT OF VOLUME COMPRESSIBILITY Mv cm3/kg
		OBSERVED VALUE	CORRECTED VALUE	5 10 20		GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm3)	DRY DENSITY(gm/cm3)			TYPE OF TEST	COHESION c (kg/cm2)	ANGLE OF FRICTION IN DEGREE	VOID RATIO eo	COMPRESSION INDEX Cc		
UDS 5					Yellowish Reddish Silty clay CL																		
SPT5	7.5	19				0.4	3.4	96.2		35	19	16	1.99	1.61	23.5	2.65	UUT	0.8	13.0				
UDS 6					Yellowish Reddish Silty clay CL																		
SPT6	9.0	21				0.40	3.60	96.0		35	19	16	1.99	1.61	23.30	2.65	UUT	0.90	13.00				
UDS 7					Yellowish Reddish Silty clay CL																		
SPT7	10.5	26				0.40	3.60	96.0		35	19	16	1.99	1.61	23.50	2.65	UUT	0.90	13.00				

UUT : UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST

UCT : UNCONFINED COMPRESSION SHEAR TEST

DST : DIRECT SHEAR TEST

! SAMPLE SLIPED

~ TEST ON REMOULDED SAMPLE

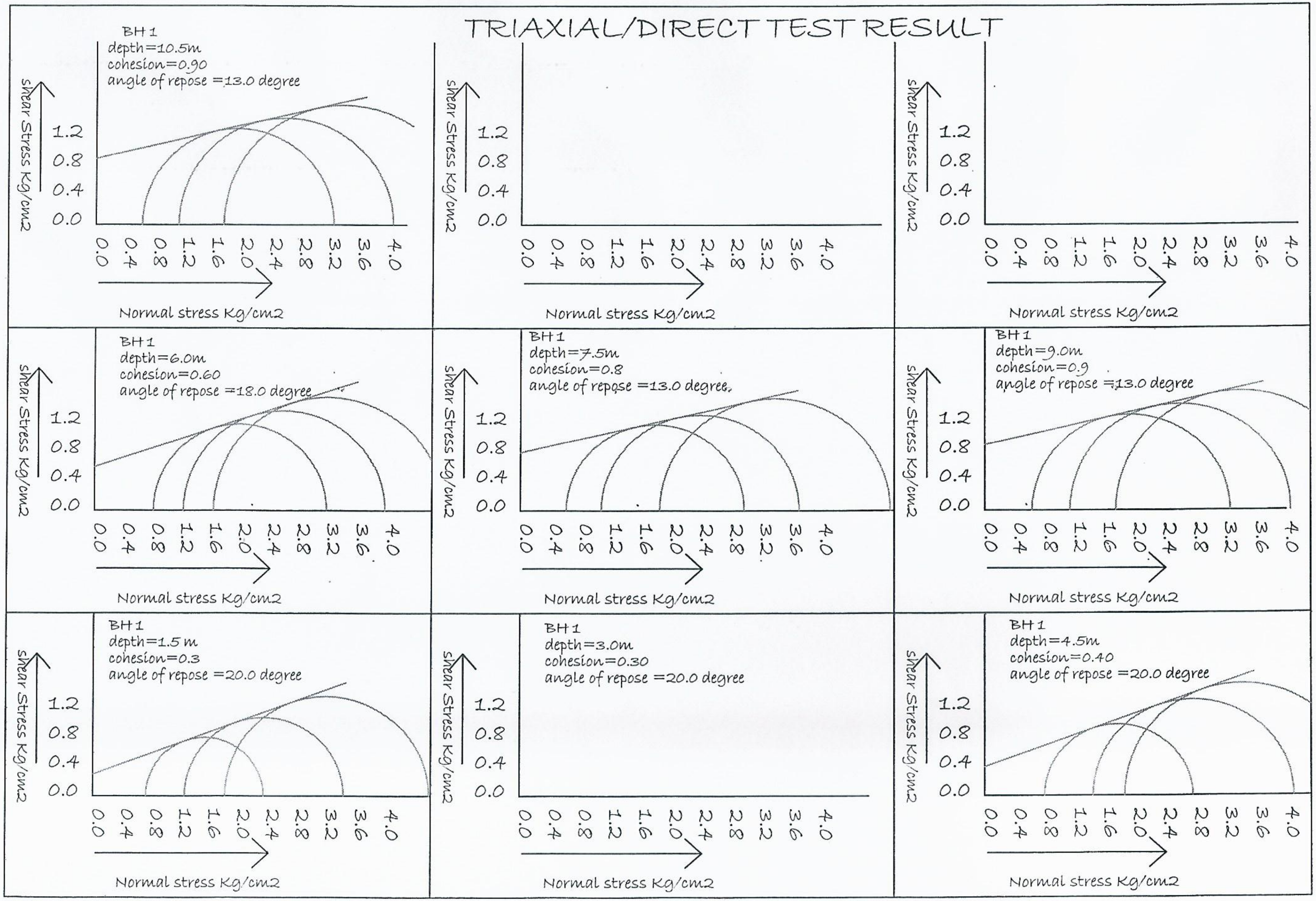
UDS : UNDISTURBED SAMPLE

SPT : STANDARD PENETRATION TEST VALUE

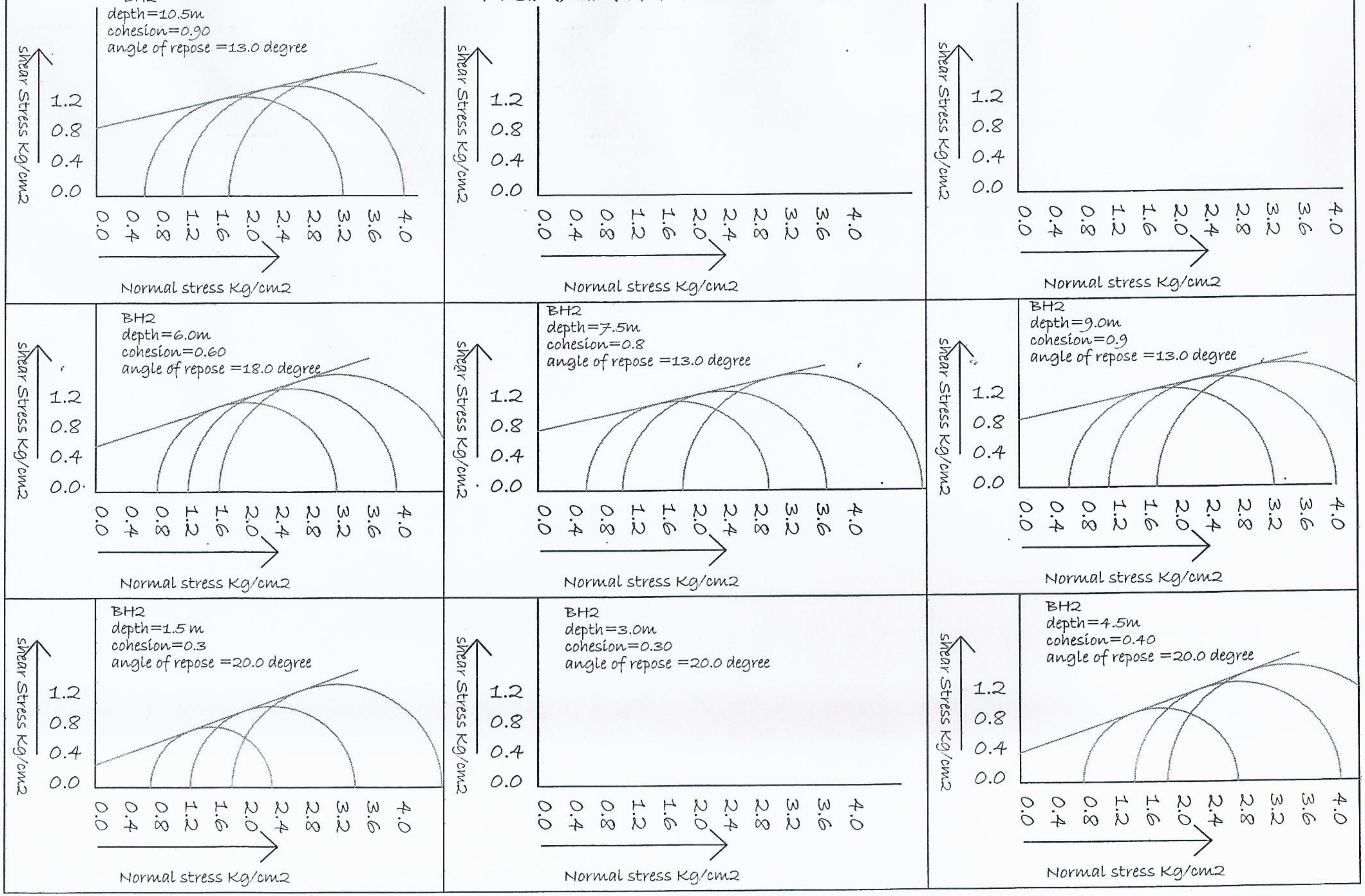
NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m2

GIRL,BOY HOSTEL EDUCATIONAL BHAWAN, PRINCIPAL-CUM-STAFF QUARTER BUILDING(G+4) AT PTEC MOKAMA,PATNA,BI

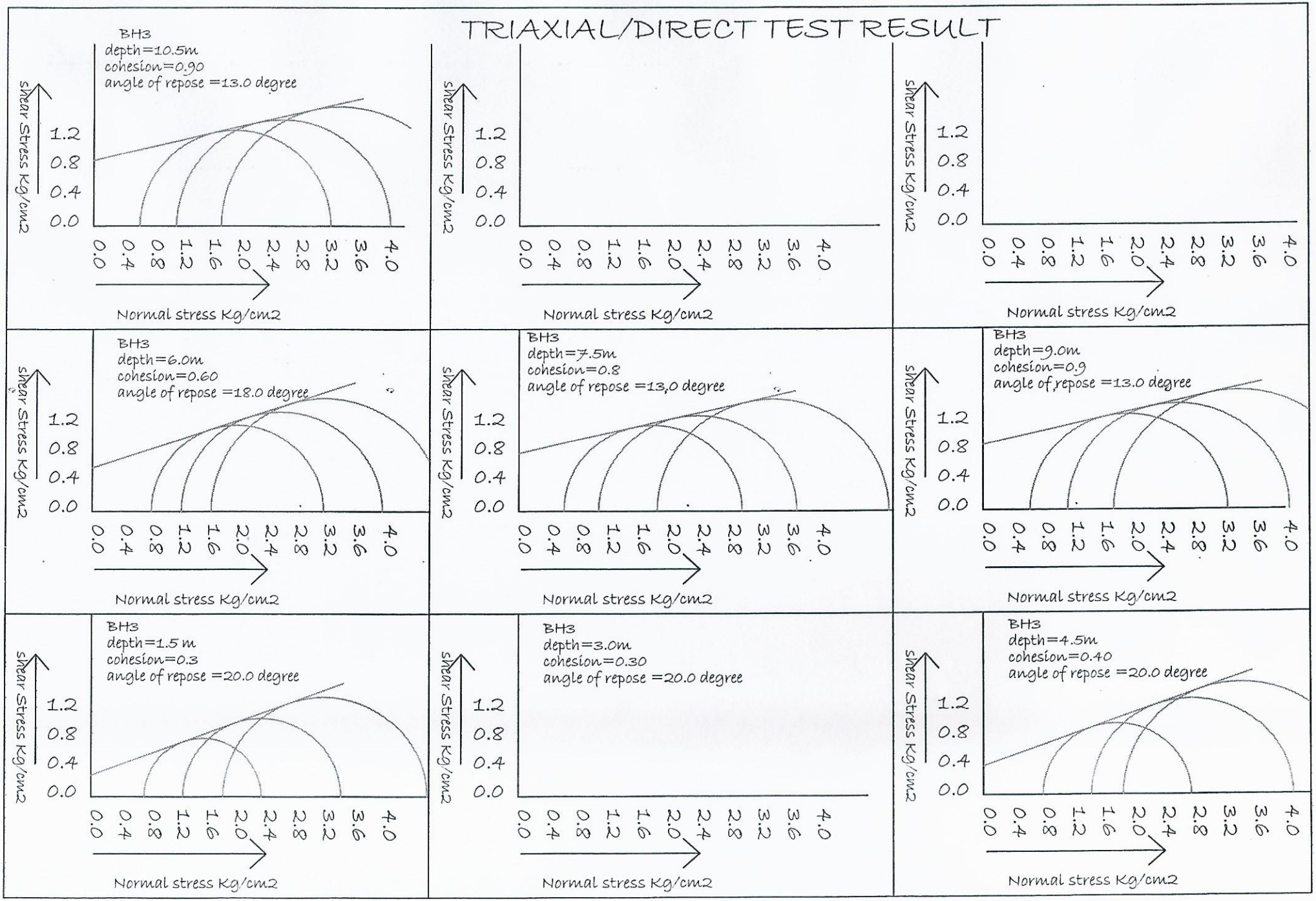
TRIAXIAL/DIRECT TEST RESULT



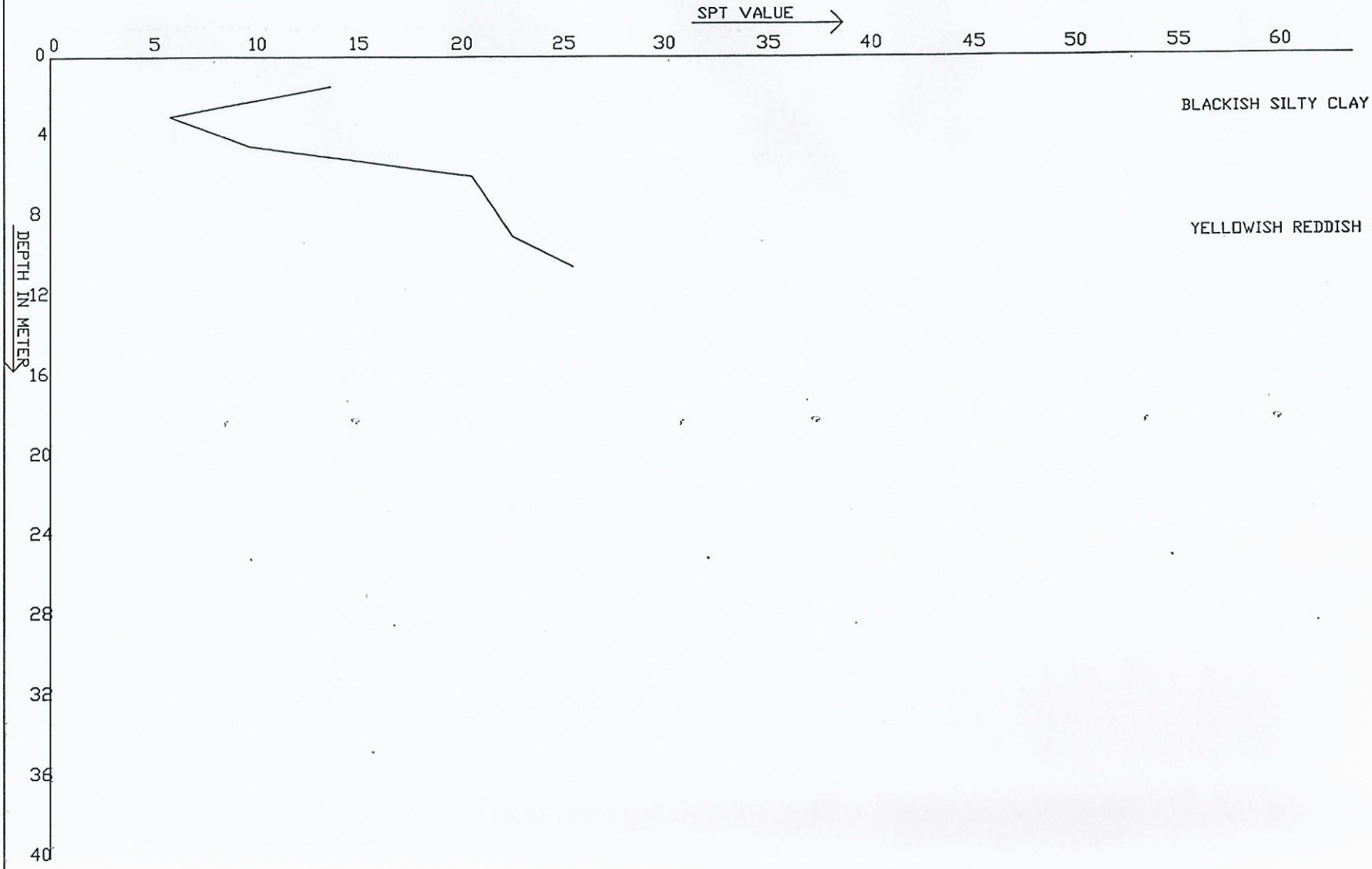
TRIAXIAL/DIRECT TEST RESULT

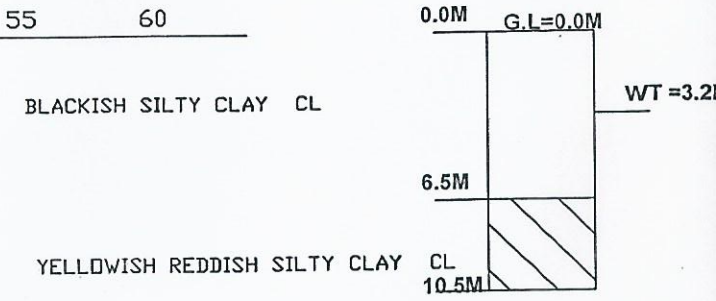


TRIAXIAL/DIRECT TEST RESULT



BORE LOG AND DEPTH ~ SPT GRAPH (GIRL,BOY HOSTEL EDUCATIONAL BHAWAN etc.(G+4) AT PTEC MOKAMA,PATNA,BIHAR





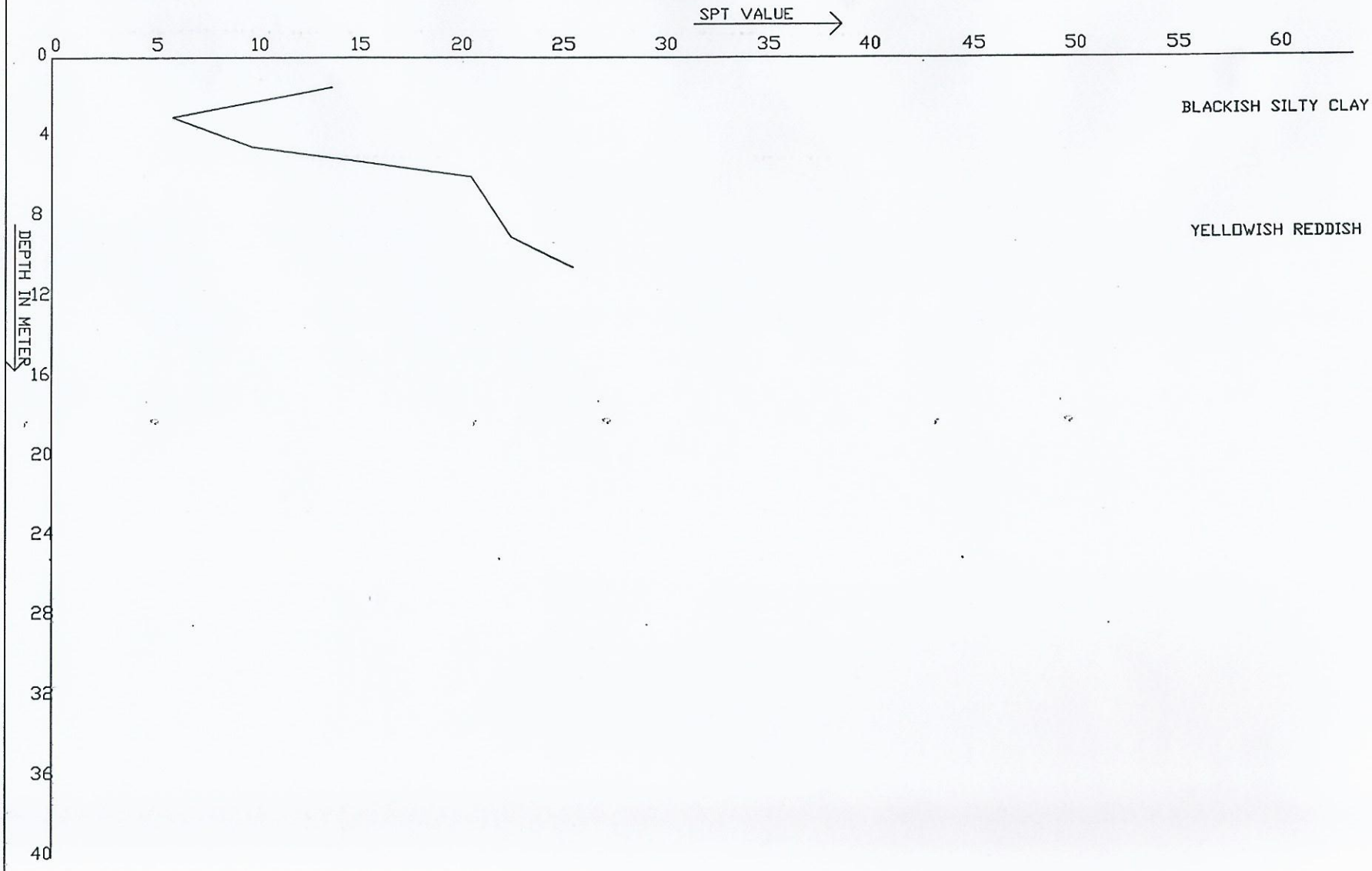
BLACKISH SILTY CLAY CL

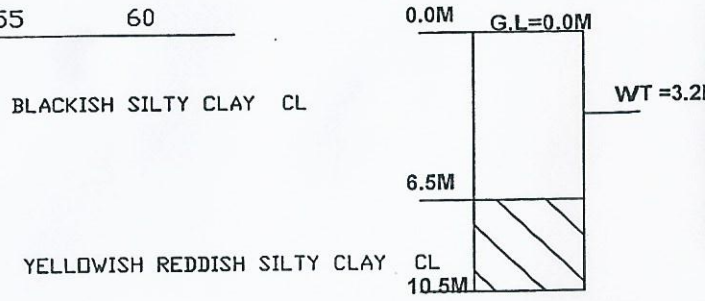
YELLOWISH REDDISH SILTY CLAY CL

BORE LOG

BH1

BORE LOG AND DEPTH ~ SPT GRAPH (GIRL,BOY HOSTEL EDUCATIONAL BHAWAN etc.(G+4) AT PTEC MOKAMA,PATNA,BIHAR

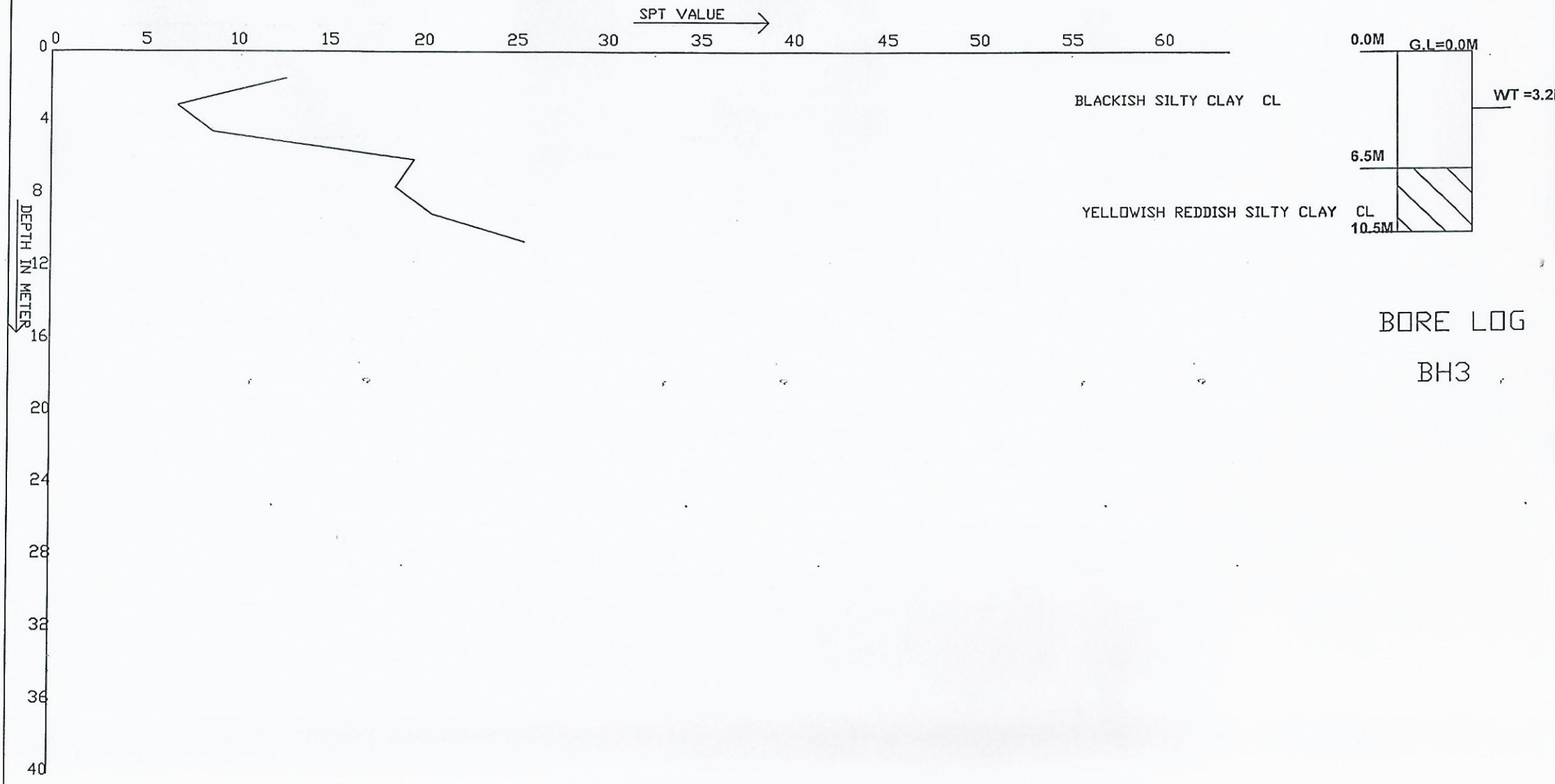




BORE LOG

BH2

BORE LOG AND DEPTH ~ SPT GRAPH (GIRL,BOY HOSTEL EDUCATIONAL BHAWAN etc.(G+4) AT PTEC MOKAMA,PATNA,BIHAR

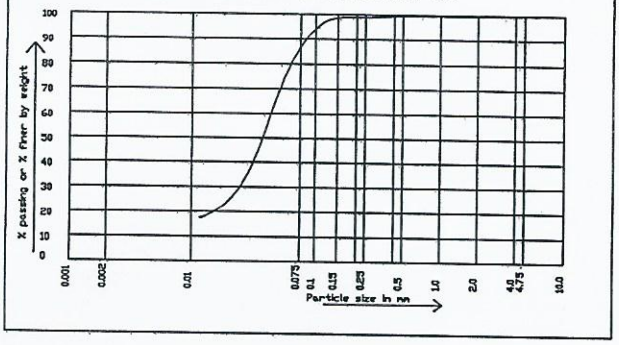


BORE LOG

BH3

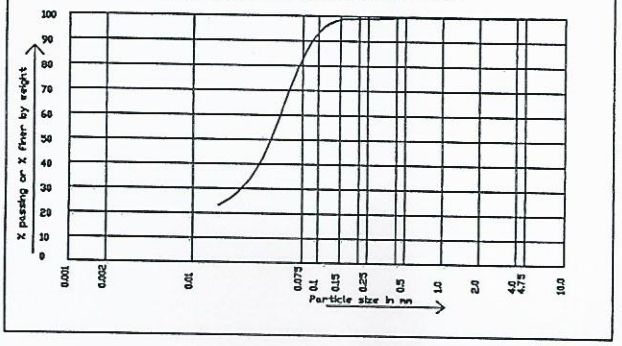
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =1.5m)



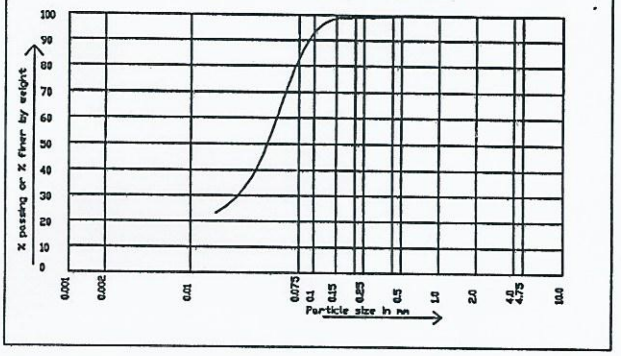
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =3.0m)



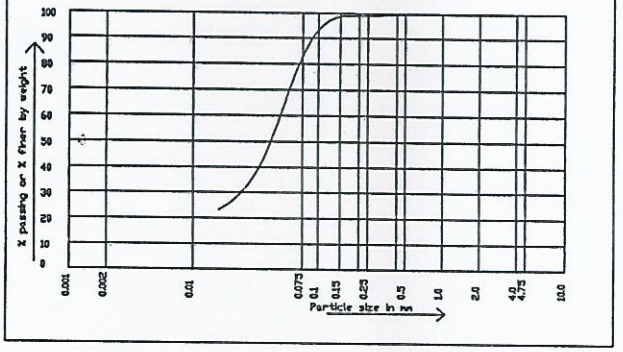
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =4.5m)



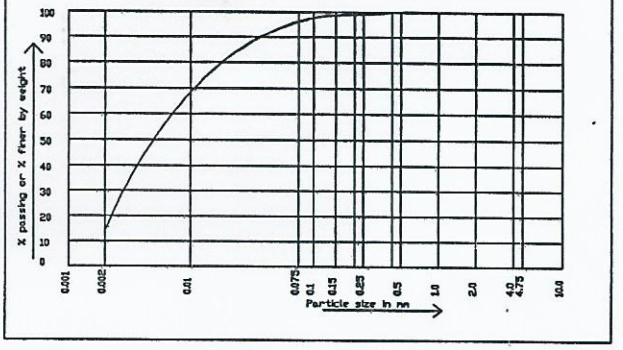
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =6.0m)



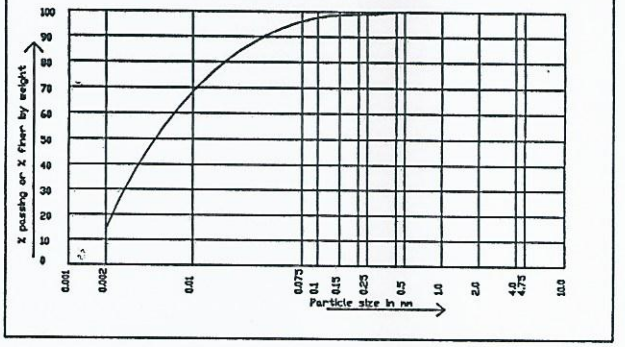
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =7.5m)



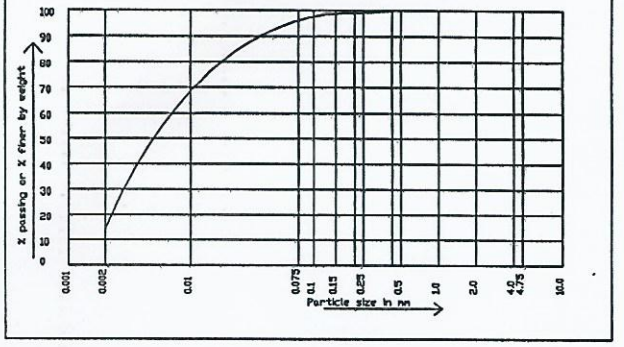
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

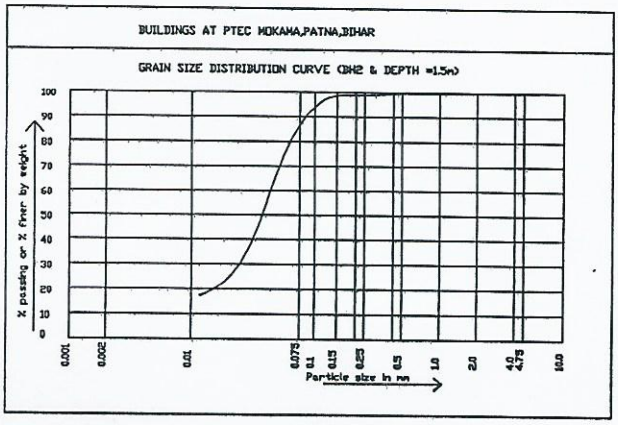
GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =9.0m)

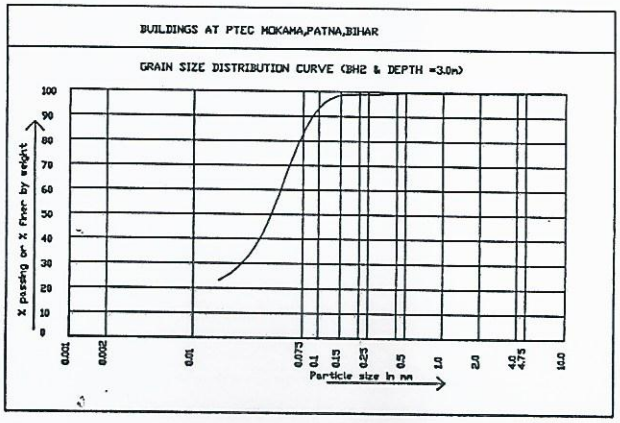


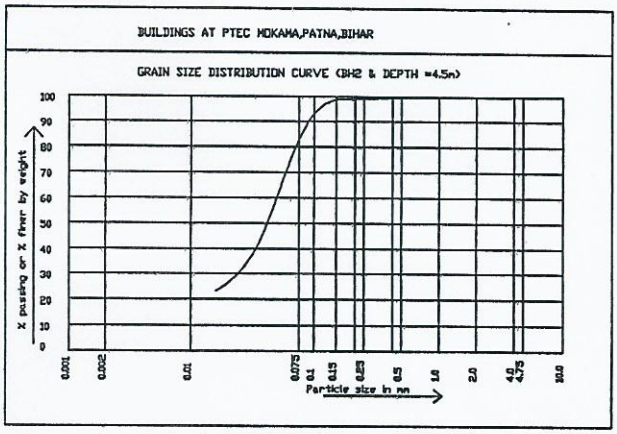
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

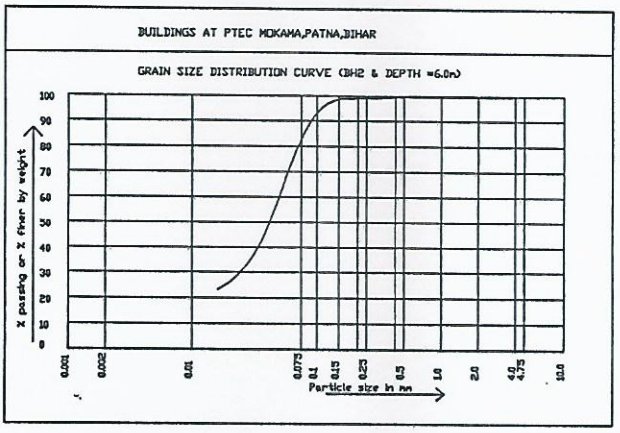
GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =10.5m)

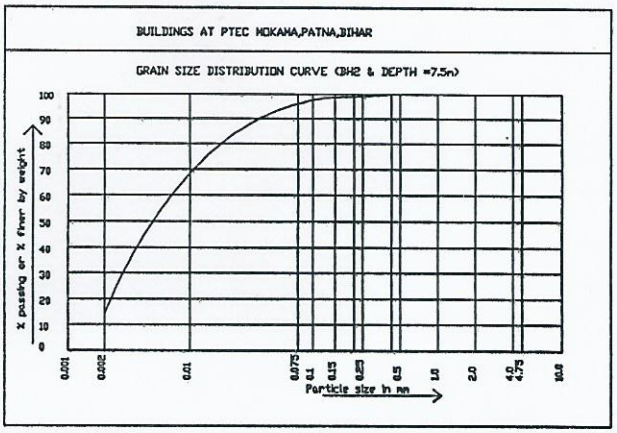


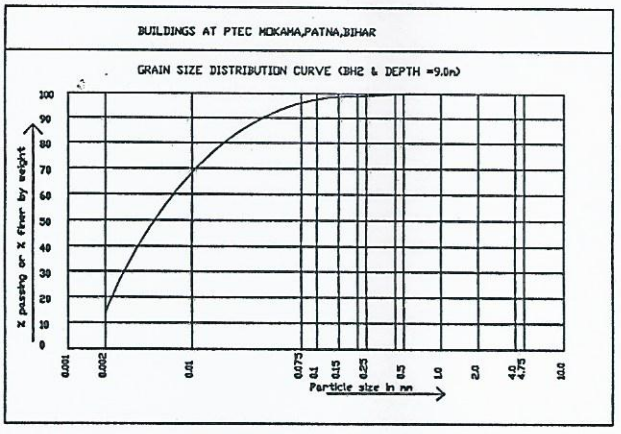

BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR
GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =1.5m)
X passing or X finer by weight
Particle size in mm

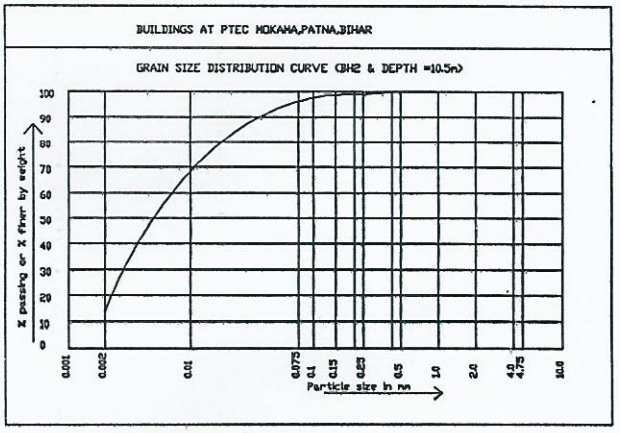

BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR
GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =3.0m)
X passing or X finer by weight
Particle size in mm


BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR
GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =4.5m)
X passing or X finer by weight
Particle size in mm


BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR
GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =6.0m)
X passing or X finer by weight
Particle size in mm

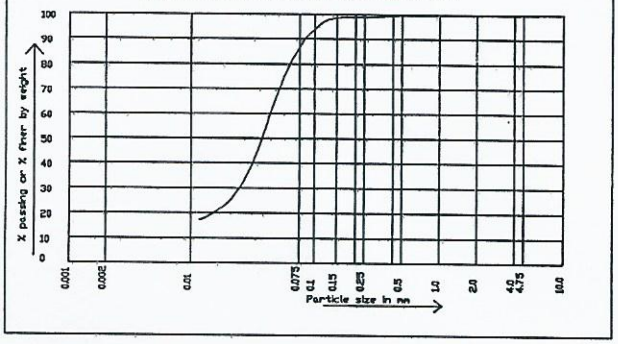

BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR
GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =7.5m)
X passing or X finer by weight
Particle size in mm


BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR
GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =9.0m)
X passing or X finer by weight
Particle size in mm


BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR
GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =10.5m)
X passing or X finer by weight
Particle size in mm

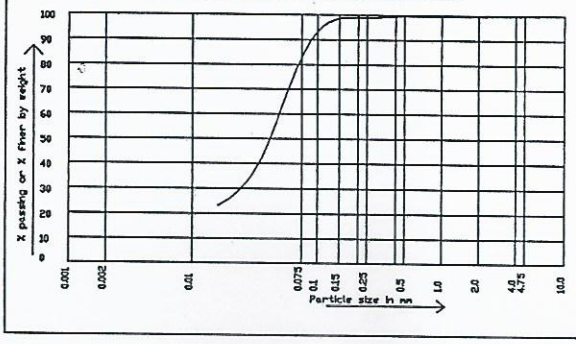
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =1.5m)



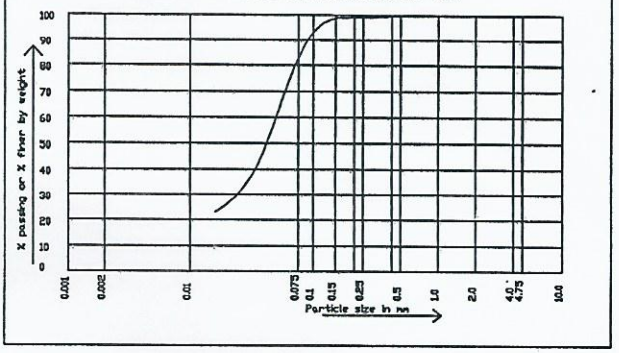
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =3.0m)



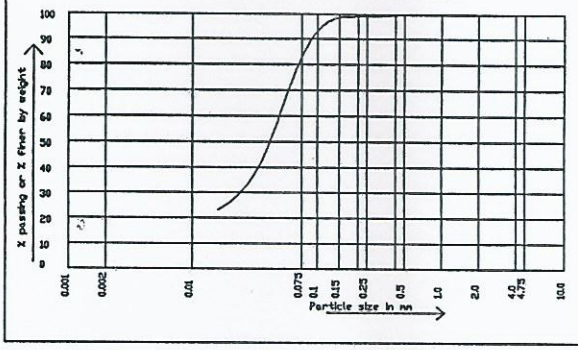
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =4.5m)



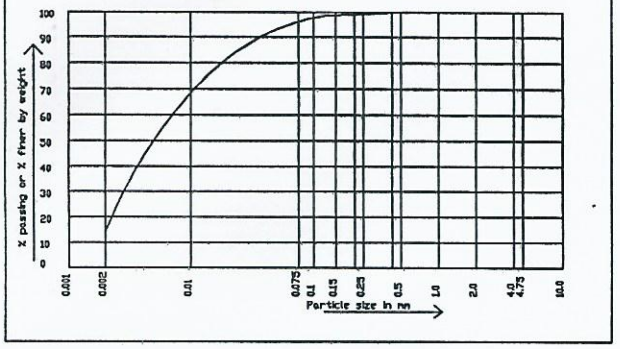
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =6.0m)



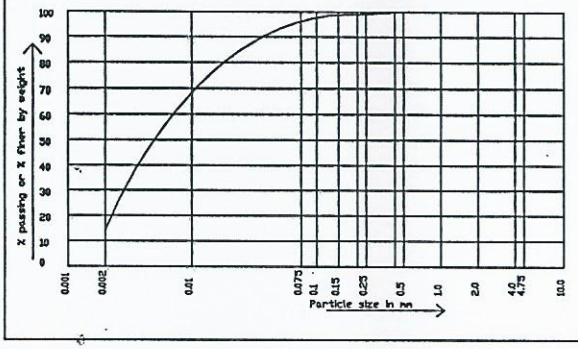
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =7.5m)



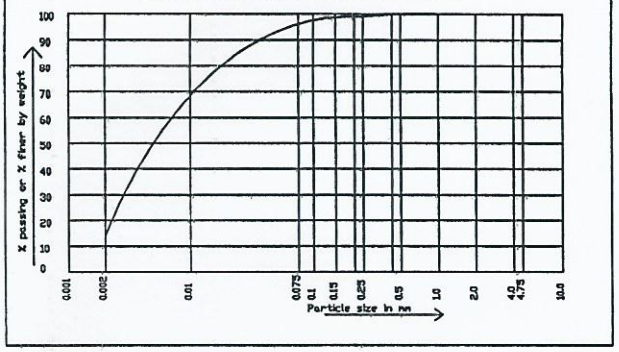
BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =9.0m)



BUILDINGS AT PTEC MOKAMA,PATNA,BIHAR

GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =10.5m)



NAME OF PROJECT : SOIL INVESTIGATION FOR CONSTRUCTION OF GIRL,BOYHOSTEL EDUCATIONAL BHAWAN, PRINCIPAL-CUM-STAFF QUARTER BUILDING(G+4) AT PTEC MOKAMA,PATNA,BIHAR

Calculation of Net safe Bearing Capacity for Strip Footing

Table 1 BEARING CAPACITY FACTORS AS PER IS 6403 : 1981

Angle of shearing resistance of soil, phi	Nc	Nq	Ny
0	5.14	1	0
5	6.49	1.57	0.45
10	8.35	2.47	1.22
15	10.98	3.94	2.65
20	14.83	6.4	5.39
25	20.72	10.66	10.88
30	30.14	18.4	22.4
35	46.12	33.3	48.03
40	75.31	64.2	109.41
45	138.88	134.88	271.76
50	266.89	319.07	762.89

Depth of footing below GL in	1.5			Water Table assumed=	1.5	m
Width of footing in meter,B=	3					
Effective depth of soil formation	3.5					
Average cohesion of soil mobilised in Ton/m2=	3.00					
unit weight of soil in ton/m2,y=	1.98					
Angle of shearing resistance of soil, phi,in degree =	20.00	Corresponding Nc/N'c=	10.30	Corresponding Nq/N'q=	3.56	Corresponding Ny/N'y= 2.28
Effective Angle of shearing resistance of soil, phi,in degree =	13.70	Corresponding Nc/N'c=	10.30	Corresponding Nq/N'q=	3.56	Corresponding Ny/N'y= 2.28
Depth factor,dc=	1.13	dc=1+0.2*(Df/B)*tan(45+phi/2)				
Depth factor,dq=	1.06	dq=1+0.1*(Df/B)*tan(45+phi/2) if phi >10 otherwise dq=1				
Depth factor,dy=	1.06	dy=1+0.1*(Df/B)*tan(45+phi/2) if phi >10 otherwise dy=1				
effective surcharge at base level of foundation,q=yD	3.0	q=yD				
Q1 ton/m2 =	23.28	Q1=(2/3)*c*N'c*dc		Bearing capacity from Fig 9 of above code=	12	t/m2
Q2 ton/m2 =	8.14	Q2=q*(N'q-1)*dq				
Q3 ton/m2 =	1.78	Q3=(1/2)*B*y*N'y*dy*W'		Min Bearing capacity=	11.1	t/m2
ultimate bearing capacity Q ton/m2 =	33.2	Q=Q1+Q2+Q3				
Factor of safety,F.S. =	3					
Net Safe Bearing Capacity in ton/m2 q=	11.1	q=Q1/F.S.				

NAME OF PROJECT : SOIL INVESTIGATION FOR CONSTRUCTION OF GIRL,BOYHOSTEL EDUCATIONAL BHAWAN, PRINCIPAL-CUM-STAFF QUARTER BUILDING(G+4) AT PTEC MOKAMA PATNA BIHAR

Calculation of settelement in clay for Strip Footing as per IS : 8009 (Part I)-1976 (Reaffirmed 1993)

Width of FOOTING in meter	3.00							
bearing capacity of soil in ton /m2 =	8							
Unit weight of soil in ton/m2 =	1.98							
Height of compressible soil in meter =H	4.50	Assuming 2:1 pressure distribution						
initial void ratio e0=	0.83							
Compression index Cc=	0.11							
Depth of Foundation in meter=	1.5							

Determination of Bearing pressure at different depth below footing level factor for Strip footing

Initial Effective stress at the top of clay layer=po	2.97	t/m2	
It is assumed that water table does not goes above footing level.			
Initial Effective stress at the bottom of clay layer=po	7.38	t/m2	
Average Effective stress on the clay stratum before construction=	5.18	t/m2	p0
Additional Stress at the top of stratum due to construction=	8	t/m2	
Additional Stress at the bottom of stratum due to construction=	3.20	t/m2	
Additional Stress at the center of stratum due to construction=	4.571	t/m2	
Hence Average effective stress on the clay stratum after construction=		9.8	(p0+p1)

Settelement s in mm =s=H/(1+e0)*Cc*Log10((po+p1)/p0)=0.11X4500X(LOG10(9.8/5.18))/(1+0.83)=

Settelement s in mm =s=H/(1+e0)*Cc*Log10((po+p1)/p0)	74.9	
D/sqrt(L*B)	0.87	
Final D/sqrt(L*B)=	0.87	
L/B=	3.00	
Depth Factor=	0.97	
Correction for normally consolidated soil=	0.8	
Correction for rigidity=	1	
Corrected Settelement s in mm=	58	

SAMPLE CALCULATION OF CAPACITY OF UNDER REAM PILE for Cohesion							NAME OF PROJECT : SOIL INVESTIGATION FOR C/O GIRL BOY HOSTEL EDUCATIONAL BHAWAN, PRINCIPAL-CUM-STAFF QUARTER BUILDING(G+4) AT PTEC MOKAMA,PATNA,BIHAR					
The load carrying capacity of the pile has been calculated using IS : 2911 (Part III) 1980,Clause 5.2.3.1												
These calculations are based on												
(a) in fine- grained soils, only on cohesion (c). In t/m², taking angle of internal friction = 0												
This is likely to give the minimum capacity of the pile												
Pile diameter, D (m) =	0.4	Hence, area of pile base. Ap (m²) =			0.126	& circumference (in m) of pile base j =			1.256			
Under ream, diameter, Du (m) =	1	Hence, Aa (m²) =	0.66	Spacing between under ream in m =		1.50	Hence, A's (m²) =		4.71			
The following values are taken in view of the codal provisions :							Surface area of pile's contact with soil, As (m²) = j x t					
Reduction factor, α, depending on N.	0.5						where t = thickness of soil layer in contact with pile.					
Skin friction in clay, Qs = α *Ca*As.	Total Ultimate capacity of pile, Qu = Ap*Nc*Cp + Aa*Nc*C'a +C'a*A's											
Total Ultimate capacity of pile, Qu = Ap*Nc*Cp + Aa*Nc*C'a +C'a*A's + Qs						Nc=	9					
Safe capacity of pile, Qsf = Qs / 3.0 + Qb / 3.0,						Reduction factor for water=α=			0.6			
takeing factor of safety =	2.5											
Depth of soil layer (m)	Soil type	Average cohesion Ca	cohesion cp t/m²	Thickness of layer, t [m]	Average cohesion C'a	As = m²	αAp*Nc*Cp I	αAa*Nc*C'a II	αC'a*A's III	Qs = α *Ca*As IV	Ultimate capacity (TON)	Safe capacity (TON)
8	clay	4.8	8	8	7	8.16	5.44	24.95	19.78	19.58	69.75	27.90

Table 8

Soil stratification

DEPTH	SOIL TYPE	CONSISTANCY	CLASSIFICATION
0.0-6.5	BLACKISH SILTY CLAY	MEDIUM	CL
6.5-10.5	REDDISH SILTY CLAY	MEDIUM TO STIFF	CL

WATER TABLE was found at 3.2m as reported in September'2023.

RECOMMENDATION

The present report is prepared on the basis of lab. Test result & field test conducted in the field.

The lab. Test result is obtained by conducting different test on representative sample obtained through 3 no. of bore holes whose location and depth were decided by Engineer-in-charge of the department and shown in the bore hole location plan. These Boreholes are marked as BH1, BH2 and, BH3.

The laboratory test of soil samples obtained in all bore holes are given in Tables 2-7.Study of these tables reveals :

(a) Strata up to 10.5m consist of fine grained soil.

Both Shallow as well as pile foundation is feasible for the site. Bentonite or casing may be suggested to prevent the collapse of pile bore. Since, Permissible differential settlement depends on the structural parameters such as structural system, span etc., these can be obtained from the IS 1904, 1986.

By way of example the calculated value of safe capacity of certain diameter of piles using IS : 2911 (Part III) 1980: -

Double Under-reamed Pile Capacity

Depth of Pile below GL(m)	Dia of Pile (m)	Dia of Under-reamed (m)	Allowable Capacity (Ton)
8.0	0.3	0.75	16
8.0	0.4	1.0	24

By way of example the calculated value of safe capacity of certain type and size of Shallow foundation are being tabulated below: -

Shallow foundation

Depth below GL (m)	Width of foundation (m)	Allowable bearing capacity(t/m2)	Maximum expected settlement(mm)
1.5	3.0	8.0	60
2.0	2.0	9.0	60

Limitation

If the sub-soil condition is found much different from those reported here during trenching, suitable steps should be taken. Back filling over footing shall be done with proper compaction.

Pile capacity shall be confirmed by Initial and Routine pile load test as per relevant Indian codes.

Subodh Kumar Sinha

SUBODH KUMAR SINHA
Partner Shamvwi consultant